

Line Losses in the 14-Bus Power System Network using UPFC

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Abstract—Controlling power flow in modern power systems can be made more flexible by the use of recent developments in power electronic and computing control technology. The Unified Power Flow Controller (UPFC) is a Flexible AC transmission system (FACTS) device that can control all the three system variables namely line reactance, magnitude and phase angle difference of voltage across the line. The UPFC provides a promising means to control power flow in modern power systems. Essentially the performance depends on proper control setting achievable through a power flow analysis program. This paper presents a reliable method to meet the requirements by developing a Newton-Raphson based load flow calculation through which control settings of UPFC can be determined for the pre-specified power flow between the lines. The proposed method keeps Newton-Raphson Load Flow (NRLF) algorithm intact and needs little modification in the Jacobian matrix). A MATLAB program has been developed to calculate the control settings of UPFC and the power flow between the lines after the load flow is converged. Case studies have been performed on IEEE 5-bus system and 14-bus system to show that the proposed method is effective. These studies indicate that the method maintains the basic NRLF properties such as fast computational speed, high degree of accuracy and good convergence rate.

Index Terms—FACTS (Statcom, TCSC) - Optimal power flow algorithm (N-R Method) – Mat lab

I. INTRODUCTION

As the power systems are becoming more complex it requires careful design of the new devices for the operation of controlling the power flow in transmission system, which should be flexible enough to adapt to any momentary system conditions. The operation of an ac power transmission line, is generally constrained by limitations of one or more network parameters and operating variables by using FACTS technology such as STATCON (Static Condenser), Thyristor Controlled Series Capacitor (TCSC), Thyristor controlled Phase angle Regulator (TCPR), UPFC etc., the bus voltages, line impedances, and phase angles in the power system can be regulated rapidly and flexibly. FACTS do not indicate a particular controller but a host of controllers which the system planner can choose based on cost benefit analysis. The UPFC is an advanced power system device capable of providing simultaneous control of voltage magnitude and active and reactive power flows in an adaptive fashion. Owing to its

instantaneous speed of response and unrivalled functionality, it is well placed to solve most issues relating to power flow control in modern power systems. The UPFC can control voltage, line impedance and phase angles in the power system [1] which will enhance the power transfer capability and also decrease generation cost and improve the security and stability (which is out of the scope of the paper) of the power system. UPFC can be used for power flow control, loop flow control, load sharing among parallel corridors.

In this paper UPFC is treated to operate in closed loop form and control parameters of UPFC are derived to meet the required power flow along the line.

II. UPFC MODEL FOR POWER FLOW STUDIES

A. Principles Of UPFC

The UPFC can provide simultaneous control of transmission voltage, impedance and phase angle of transmission line. It consists of two switching converters as shown in fig 1. These converters are operated from a common d.c link provided by a d.c storage capacitor. Converter 2 provides the power flow control of UPFC by injecting an ac voltage V_{pq} with controllable magnitude and phase angle in series with the transmission line via a series transformer. Converter 1 is to absorb or supply the real power demand by the converter 2 at the common d.c link. It can also absorb or generate controllable reactive power and provide shunt reactive power compensation. The UPFC concept provides a powerful tool for cost effective utilization of individual transmission lines by facilitating the independent control of both the real and reactive power flow and thus the maximization of real power transfer at minimum losses in the line [5] This is the topic of this paper.

B. Power injection model of UPFC

The two voltage source model of UPFC is converted in to two power injections in polar form for power flow studies with approximate impedances as shown in fig 2. The advantage of power injection representation is does not destroy the symmetric characteristics of admittance matrix. When formulated in polar form, the power flow equations are quadratic. Some numerical advantages can be obtained from the form. The polar form also leads naturally to the idea of an optimal power flow, which will be discussed in next section.

The voltage sources can be represented by the relation-

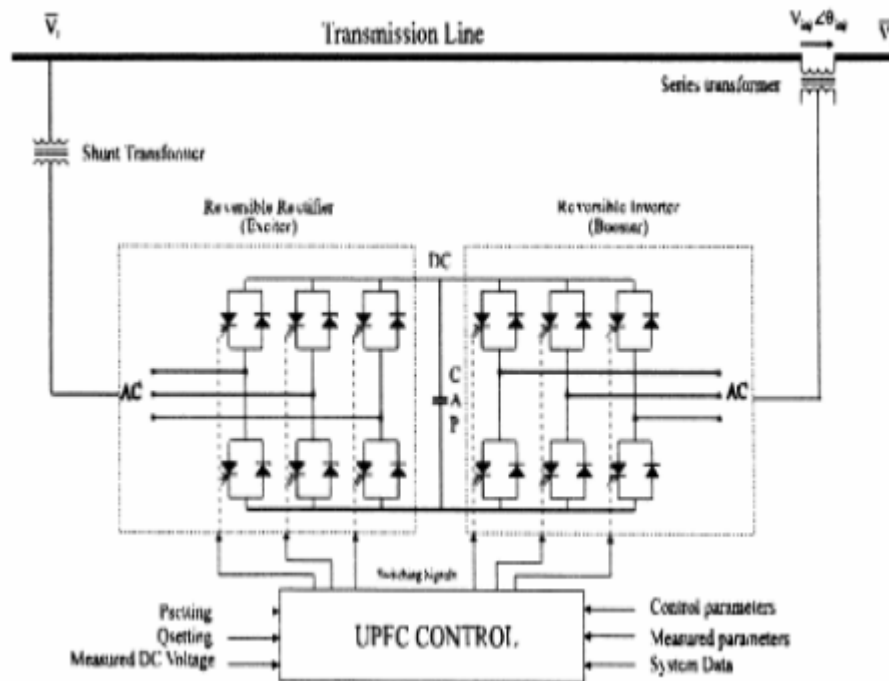


Fig.1 Implementation of the UPFC by back-to-back voltage source converters

ship between the voltages and amplitude modulation ratios and phase shift of UPFC. In this model the shunt transformer impedance and the transmission line impedance including the series transformer impedance are assumed to be constant. No power loss is considered with the UPFC. However the proposed model and algorithm will give the solution of optimal power flow in the transmission

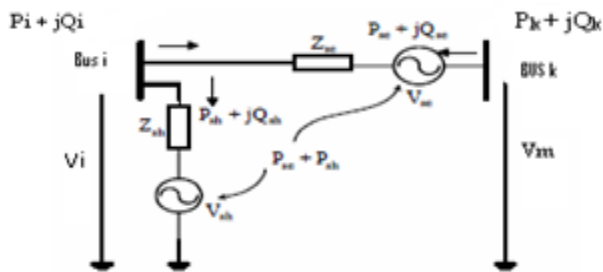


Fig.2. Two Voltage source model of UPFC

C. Steady state UPFC representation

There are two aspects in handling the UPFC in steady state analysis.

1. When the UPFC parameters are given, a power flow program is used to evaluate the impact of the given UPFC on the system under various conditions. In this case UPFC is operated in open loop form. The corresponding power flow is treated as normal power flow(Which is the out of the scope of the paper).
2. As UPFC can be used to control the line flow and bus voltage, control techniques are needed to derive the UPFC control parameters to achieve the required objective. In this case UPFC is operated in closed loop form. The corresponding power flow is called controlled power flow. This is the topic of this paper.

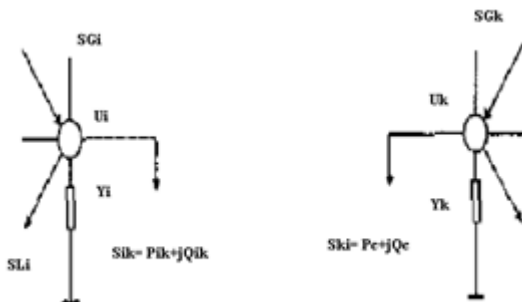


Fig.3: steady state model of UPFC connected between bus 1 and m

For a given control strategy, the power S_{m1} on the UPFC-controlled transmission line i-k is set to constant ($P_c + jQ_c$). By means of the substitution theorem, this branch i-k can be detached as shown in Fig.3. in which S_{ki} represents power from the bus k and S_{ik} from the bus i. For each other additional UPFC, its corresponding branch can be dealt with similarly.

III. PROBLEM FORMULATION OF UPFC FOR POWER FLOW STUDIES

A. Load flow problem

In this paper the load flow problems are solved by using N-R method in polar co-ordinate form is an iterative method which approximates the set of linear simultaneous equations using Taylor's series expansion and the terms are limited to first approximation. In the power flow of the transmission line the complex power injected at the i^{th} bus with respect to ground system is

$$S_i = P_i + jQ_i \quad \dots (3.1)$$

$$= V_i I_i^* \quad \dots (3.2) \quad \text{Where } i=1, 2, 3, \dots, n.$$

Where V_i is the voltage at the i^{th} bus with respect to ground and I_i is the source current injected into the bus.

$$P_i + jQ_i = V_i I_i^* \quad \dots (3.3)$$

Substituting for $I_i = \sum_{k=1}^n Y_{ik} V_k$ (3.4)

Real power reactive power can now be expressed as

P_i (Real power)=

$$|V_i| \left| \sum_{k=1}^n Y_{ik} \right| |V_k| \cos(\theta_{ik} + \delta_k + \delta_i) \quad \dots (3.5)$$

Q_i (Reactive power)=

$$|V_i| \sum_{k=1}^n |V_k| \sin(\theta_{ik} + \delta_k + \delta_i) \quad \dots (3.6)$$

$i=1, 2, 3, 4, \dots, n$; slack bus

The following are the formulae of the UPFC to be involved in power flow studies. The major symbols used are :

S : Complex or Apparent power

S_{ik} : Complex power flowing from bus i to bus k

ΔS : Change in complex power

P : Real power

P_c : Pre – Specified real power

P_f : Real power flowing in the line

P_e : Difference in pre-specified an line real power

P_B : Real power supplied by booster transformer

P_E : Real power supplied by excitation transformer

P_{ik} : Real power flowing from bus i to k

ΔP : Change in real power

Q : Reactive power

Q_c : Pre specified reactive power

Q_f : Reactive power in line

Q_e : Difference in pre specified and line reactive power

Q_{ik} : Reactive power flowing from bus i to k

Q_B : Reactive power supplied by booster transformer

Q_E : Reactive power supplied by excitation transformer

ΔQ : Change in reactive power

V : Voltage magnitude

U_T : Injected voltage magnitude.

U_{Tmax} : Limits on injected voltage magnitude

$\Delta|V|$: Change in magnitude of voltage

δ : Phase angle of voltage

δ_{lm} : Phase angle difference between bus l and bus m

$\Delta\delta$: Change in phase angle of voltage.

Φ_T : Injected voltage phase angle

ϵ : Tolerance

I_q : Exciting transformer reactive current

Y : Admittance

θ_{ik} : Phase angle of admittance w.r.t reference

Y_{BUS} : Bus admittance matrix

Y_{ii} : Self Admittance

Y_{ik} : Mutual admittance, $i \neq k$

G_{ik} : Real part of admittance in p.u

B_{ik} : Imaginary part of admittance in p.u

J = Jacobian matrix

j : complex power” -1

m : Amplitude modulation index

R_{ik} : Resistance between bused i and k in p.u

X_{ik} : Reactance between bused i and k in p.u

B_{ik} : Line charging susceptance between i and k in p.u

Z_{ik} : Impedance between bused i and k in p.u

B. UPFC modified Jacobian matrix elements

In power flow the two power injections(P_i , Q_i) and (P_j , Q_j) as shown in fig 2 in section 2.2 of a UPFC can be treated as generators, however because they vary with the connected

bus bar voltage amplitudes and phases the relevant elements of Jacobin matrix at each iteration.

The formation of Jacobian matrix

$$\begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} = \begin{bmatrix} H & N \\ J & L \end{bmatrix} \begin{bmatrix} \Delta \delta \\ |\Delta V| \end{bmatrix}$$

Where H, N, J, L is the elements of Jacobian matrix.

$$H_{im} = \frac{\partial P_i}{\partial \delta_m}; N_{im} = \frac{\partial P_i}{\partial |V_m|}; J_{im} = \frac{\partial Q_i}{\partial \delta_m}; L_{im} = \frac{\partial Q_i}{\partial |V_m|};$$

The elements of Jacobian matrix can be calculated as follows

case1:

$m \neq i$

$$H_{im} = L_{im} = a_m f_i - b_m f_i;$$

$$N_{im} = -J_{im} = a_m e_i - b_m f_i;$$

Where

$$Y_{im} = G_{im} + jB_{im}; V_i = e_i jf_i$$

$$(a_m + jb_m) = (G_{im} + jB_{im})^* (e_i jf_i);$$

Case 2:

$$m=i, H_{ii} = -Q_i - B_{ii}|V_i|^2; N_{ii} = P_i + G_{ii}|V_i|^2;$$

$$J_{ii} = P_i - G_{ii}|V_i|^2; L_{ii} = Q_i - B_{ii}|V_i|^2$$

C. Optimal power flow Algorithm

In this paper optimal power flow algorithm is adopted as it offers a number of advantages that is to detect the distance between the desired operating point and the closest unfeasible point. Thus it provides a measure of degree of controllability and it can provide computational efficiency with out destroying the advantages of the conventional power flow when used error feedback adjustment to implement UPFC model. The proposed model and algorithm as follows.

1. Assume bus voltage V_p except at slack bus i.e.
 $p=1, 2, 3, \dots, n$; $p \neq s$ Where n is the number of buses.
2. Form Y-bus matrix.
3. Set iteration count $k=0$.
4. Set the convergence criterion, ϵ
5. Calculate the real and reactive power P_p and Q_p at each bus where $p=1, 2, 3, \dots, n$; $p \neq s$.
6. Evaluate $\Delta P_p = P_{spe} - P_p$ and $\Delta Q_p = Q_{spe} - Q_p$ at each bus where $p=1$
7. Compare each and every residue with ϵ and if all of them are $\leq \epsilon$ then go to step 13.
8. Calculate the elements of Jacobian matrix.
9. Calculate increments in phase angles and voltages.
10. Calculate new bus voltages and respective phase angles $v_p^{k+1} = v_p^k + \Delta v_p^k$ and $\theta_p^{k+1} = \theta_p^k + \Delta \theta_p^k$ where $p=1, 2, 3, \dots, n$; $p \neq s$.
11. Replace v_p^k by v_p^{k+1} and θ_p^k by θ_p^{k+1} where $p=1, 2, 3, \dots, n$; $p \neq s$.
12. Set $k=k+1$ and go to step 5 and Print the final values.

IV. CASE STUDY AND CONCLUSION

In order to investigate the feasibility of the proposed technique, a large number of power systems of different sizes and under different system conditions has been tested. It should be pointed out that the results are under so-called normal power flow, i.e. the control parameters of UPFC are given and UPFC is operated in an closed-loop form. All the results indicate good convergence and high accuracy achieved by the proposed method. In this section, the 14-bus practical system have been presented to numerically demonstrate its performance. It have been used to show quantitatively, how the UPFC performs. The original network is modified to include the UPFC. This compensates the line between any of the buses. The UPFC is used to regulate the active and reactive power flowing in the line at a pre- specified value. The load flow solution for the modified network is obtained by the proposed power flow algorithm and the Matlab program is used to find the losses between any buses and the power flow between the lines are observed the effects of UPFC. The same procedure is repeated to observe the losses between the buses. An IEEE 14 bus system is shown in below figure.9

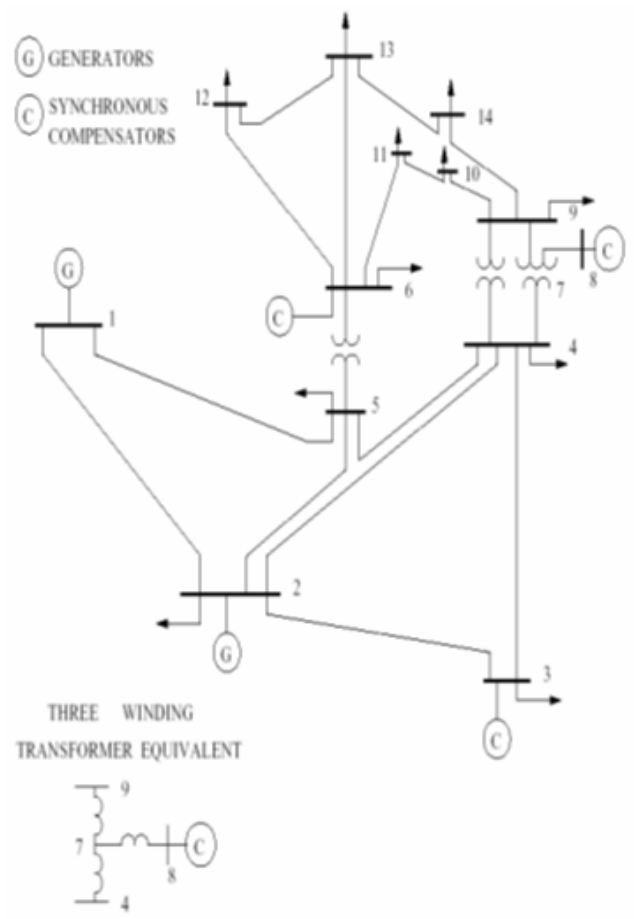


Fig 9 IEEE 14 bus system

A. Test results of voltage profile with and without UPFC for 14 bus system

The voltage profile of the 14 bus system is tabulated

TABEL:I. VOLTAGE PROFILE OF THE SYSTEM WITH AND WITHOUT UPFC

Bus code	With out UPFC			With UPFC(3 and 4)		
	Voltage(p.u)	Angle(rad)	Angle(deg)	Voltage(p.u)	Angle(rad)	Angle(deg)
1	1.06000	0.000000	0.000000	1.060000	0.000000	0.000000
2	0.17933	2.288247	131.1068	1.0137716	0.085501	4.898831
3	3.00344	2.569834	147.24067	1.0197531	0.187757	10.75769
4	0.80191	1.153725	66.103578	1.0185627	0.165721	9.495116
5	0.55792	2.134085	122.27407	1.0167506	0.142518	8.165699
6	0.36150	0.632530	36.241286	1.0206837	0.219664	12.58583
7	1.20526	0.493703	28.287102	1.0208420	0.206742	11.84544
8	0.02918	0.237284	13.595389	1.0208420	0.206742	11.84544
9	0.20075	-1.509105	-86.465347	1.0221203	0.227689	13.04560
10	0.08805	1.616350	92.610029	1.0225012	0.229993	13.17761
11	0.09586	-1.698440	-97.313422	1.0218993	0.226622	12.98449
12	0.39835	1.836755	105.23830	1.0219505	0.230963	13.23320
13	1.11687	-0.412811	-23.652326	1.0223628	0.231860	13.28461
14	0.63295	2.982683	170.89517	1.0237072	0.242100	13.87128

TABEL:II. LOSS PROFILE OF THE SYSTEM WITH AND WITHOUT UPFC

Bus code	With out UPFC	With UPFC (2 and 5)
	Loss(p.u)	Loss(p.u)
1-2	7.027357	0.074240
1-5	2.119981	0.037601
2-3	10.097645	0.020217
2-4	1.601668	0.018498
2-5	0.681603	0.008854
3-4	17.718054	0.001651
4-5	3.120731	0.007344
4-7	0.000000	0.000000
4-9	-0.000000	0.000000
5-6	0.000000	-0.000000
6-11	0.366826	0.000428
6-12	0.284050	0.000532
6-13	3.015375	0.001554
7-8	0.000000	0.000000
7-9	0.000000	0.000000
9-10	0.325453	0.000088
9-14	0.707077	0.000805
10-11	0.063149	0.000100
12-13	4.890334	0.000045
13-14	3.429823	0.000386

below for the power system network using with out and with UPFC (3 and 4)

B. Test results of power flow loss with and without UPFC for 14 bus system

The Power flow Losses of the system in between buses in the 14 bus system implementing without UPFC and with UPFC (between 2 and 5) in the network.

C. Graphical results for voltage profile and losses with and with out UPFC in 14 bus system

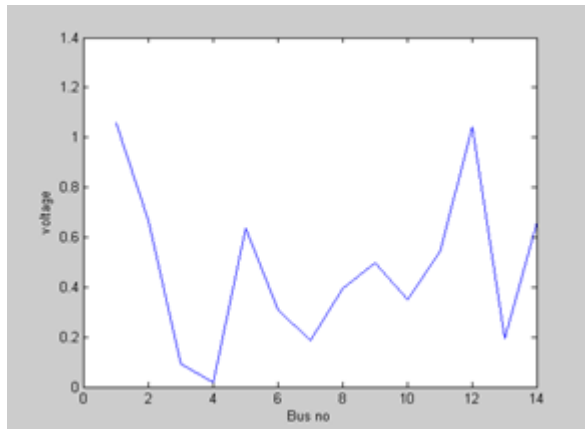


Fig 10 Voltage profile with out UPFC

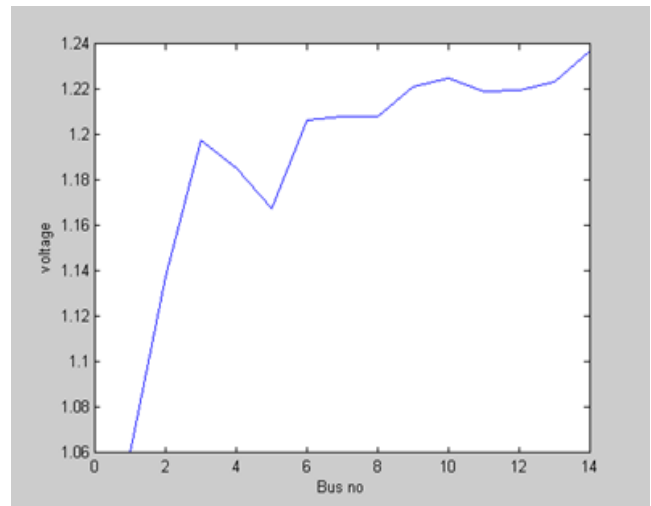


Fig 11 voltage profile with UPFC

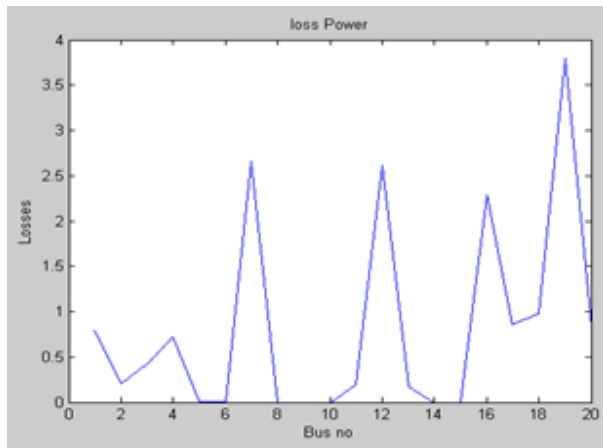


Fig 12 Loss profile with out UPFC

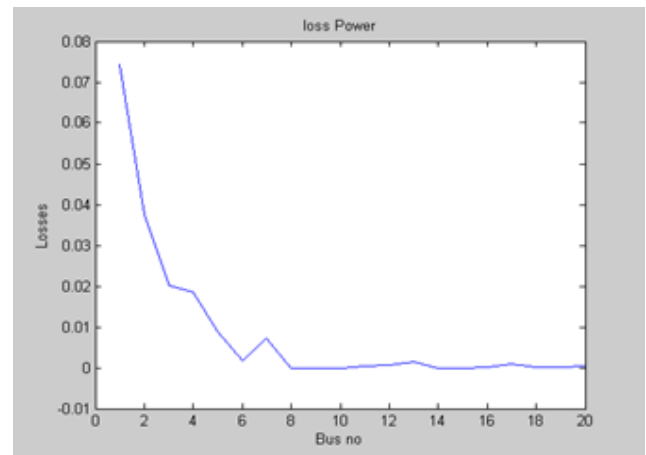


Fig 13 Loss profile with UPFC

V. CONCLUSIONS

The unified power flow controller provides simultaneous or individual controls of basic system parameters like transmission voltage, impedance and phase angle, thereby controlling transmitted power. In this thesis an IEEE 14-bus system is taken into consideration to observe the effects of UPFC. Load flow studies were conducted on given system to find the nodal voltages, and power flow between the nodes. The MATLAB program is run with and without incorporation of UPFC. The UPFC is incorporated between buses (3, 4) and (2,5) to improve the power flow between the lines to a pre-specified value. From the results it has been observed that the power flow between the lines is improved to a pre-specified value. Depending on the pre-specified value the UPFC control settings were determined. The real power losses between the lines were decreased after the incorporation of UPFC. so, it can be concluded that after the incorporation of UPFC the voltage profile and power flow between the lines improves. Also by using this program, control setting of UPFC for different pre-specified power flows can be obtained.

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BIOGRAPHIES



Mr. Sunil kumar.J (PhD) was born in Tirupathi, India. He received his B.Tech in Department of Electrical and Electronics from Anna Univeristy, Chennai, in 2006 and M.Tech from Sri Venkateswar University, Tirupathi, in 2011. Currently working as a Assistant Professor in Adama science and technology university, Adama. Currently he is pursuing his PhD. His research interests include Power Systems, Renewable Energy, Fuzzy Logic, Neural Networks, Flexible AC Transmission System (FACTS). Up to now 8 International journals are in credit, 6 International conferences. He is working as a reviewer for many journals like International Journal of Electrical Power & Energy Systems (Elsevier), International Journal of Scientific and Engineering Research, (IJ-ETA-ETS), Global Journal of Researches in Engineering, United States, International Journals of Engineering & Sciences.



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